

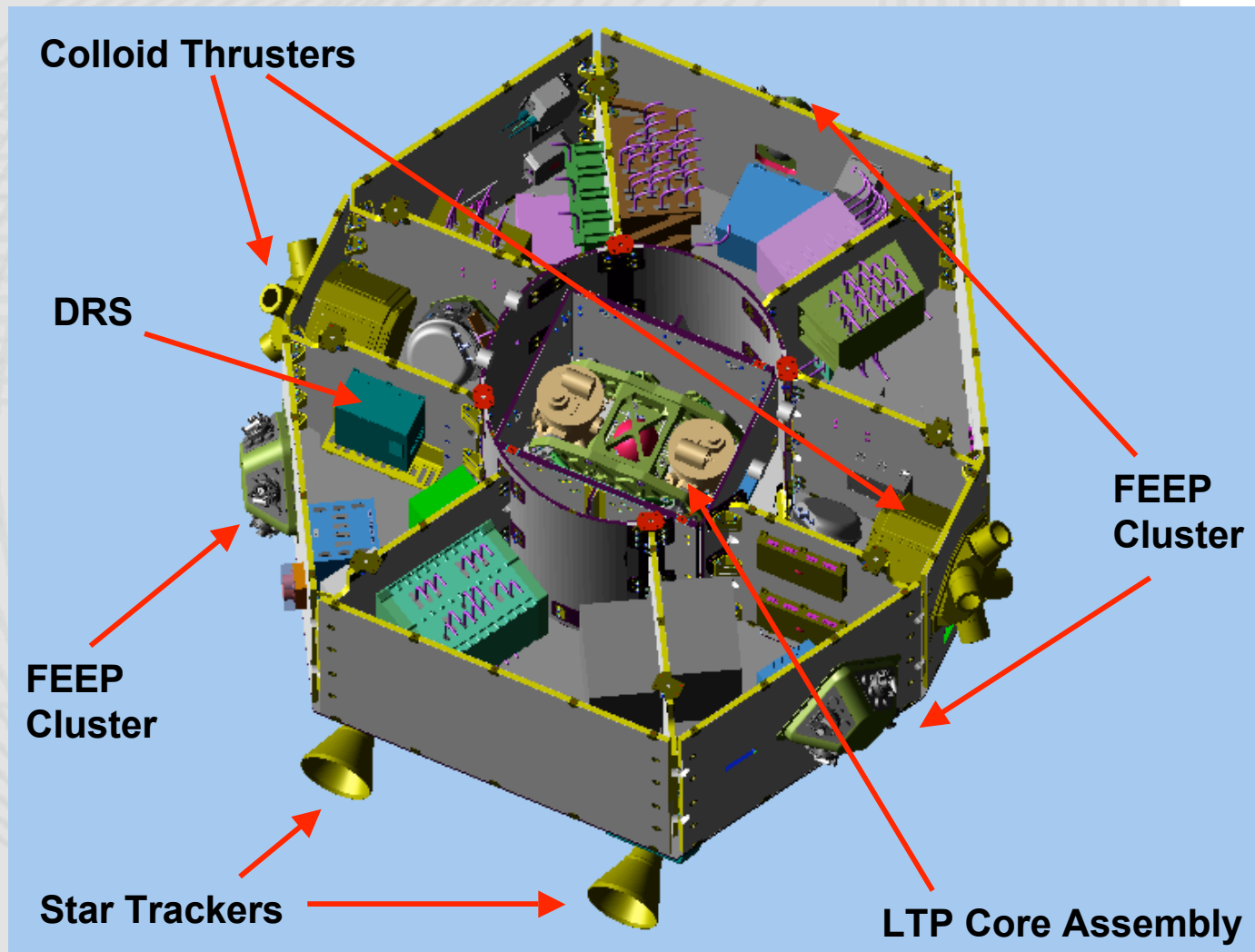
Managing Disturbances Sources on LISA Pathfinder

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Contents

- Introduction
- Self-Gravity Disturbances
- Magnetic Disturbances
- Thermal Effects
- Conclusions

LISA Pathfinder Configuration



Primary Mission Goal

- Acceleration Noise

- “*Verify that a TM can be put in pure gravitational free-fall within one order of magnitude of the requirement for LISA*”

$$S_a^{1/2}(f) \leq 3 \times 10^{-14} \left[1 + \left(\frac{f}{3 \text{ mHz}} \right)^2 \right] \frac{m}{s^2} \frac{1}{\sqrt{\text{Hz}}}$$

$$1 \text{ mHz} \leq f \leq 30 \text{ mHz}$$

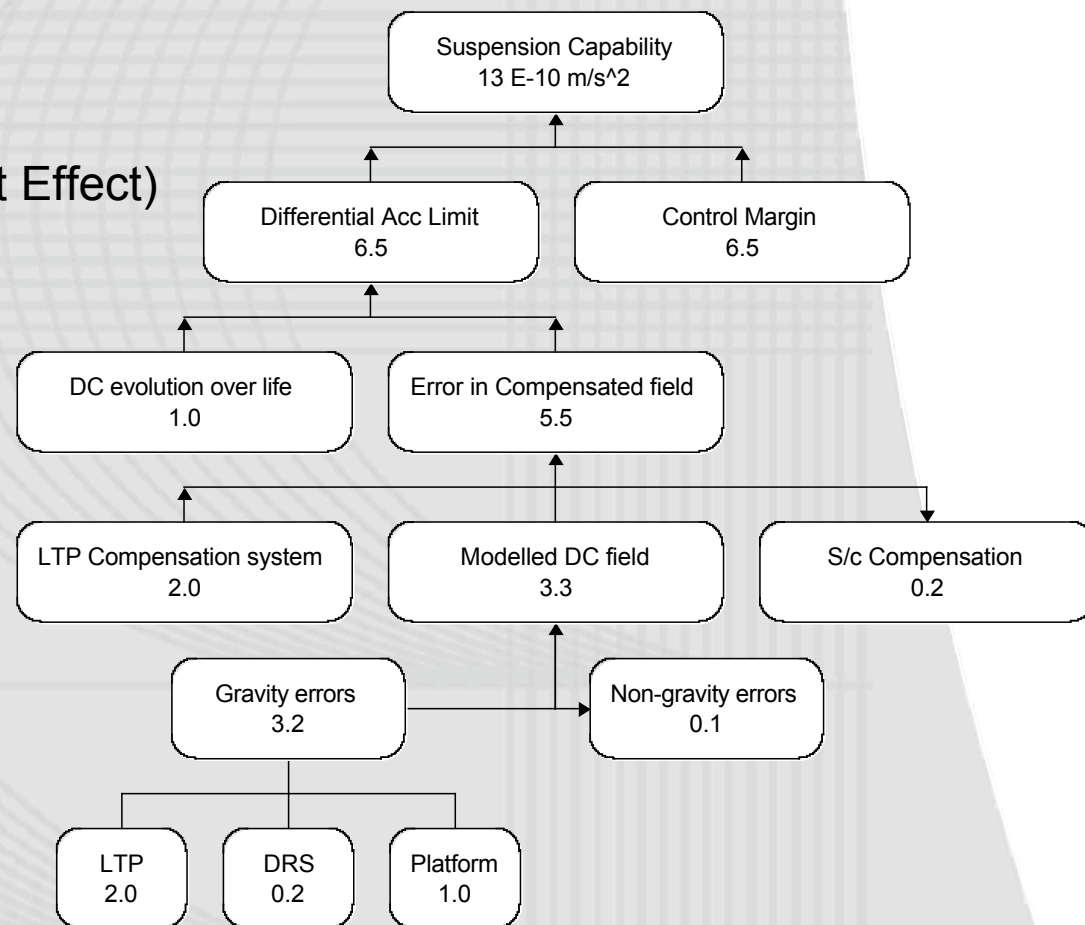
- Apportioned between known or potential disturbance sources and between contributors
 - Direct force noise caused by low frequency, time-varying forces
 - TM jitter which couples via a stiffness term
 - Optical Metrology System accuracy and alignment

Self-Gravity Disturbance Sources

- Self-gravity noise effects
 - Primarily due to thermo-elastic effects
- Actuation noise budget is $10 \times 10^{-15} \text{ m/s}^2/\sqrt{\text{Hz}}$
 - Electrostatic suspension system compensates for differential force between TM1 and TM2
 - Necessary to limit differential force and voltage fluctuations
 - 50% of budget allocated to DC force/voltage stability
- Gravity gradient stiffness effect
- Cross-coupling of forces/torques from other axes into sensitive axis

Differential DC Force

- Number of contributors to differential DC force
 - Magnetic Field
 - Electric Field
 - Thermal Effects
 - Self-Gravity (Dominant Effect)
- Natural field exceeds suspension capability
 - Balancing mandatory



Modelling Approach

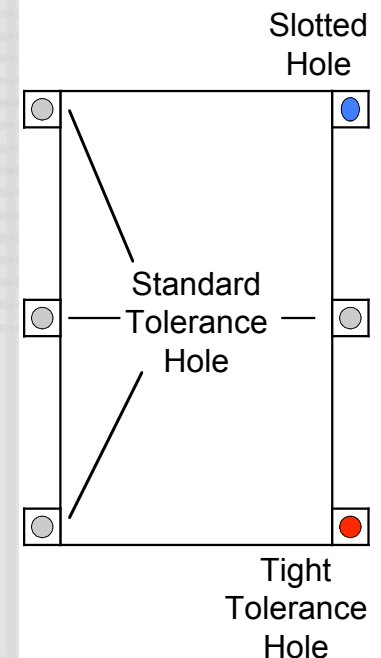
- Gravity force between source element and TMs

$$\vec{F} = \int \left(\int \vec{\nabla} \left(\frac{G \rho_{TM} \rho_{source}}{\sqrt{(x-X)^2 + (y-Y)^2 + (z-Z)^2}} \right) dV_{TM} \right) dV_{source}$$

- Two source mass modelling approaches used
 - Homogenous Source Mass
 - Integrate over test mass volume and source mass volume
 - Basic shapes – Cuboid, Cylinder, Sphere
 - Point Mass Distribution
 - Integrate over test mass volume for series of point masses
- Model output at TM1 and TM2 locations
 - Force, Torques, Force Gradients (dF/dx , $dF/d_$), Torque Gradients (dT/dx , $dT/d_$)

Minimising Equipment Location Uncertainty

- CFRP Structure minimises structure distortion
 - e.g. 0g-1g transition, outgassing and moisture loss
- Panel displacement and rotation limited
 - Displacement < 0.25 mm
 - Rotation < 0.001 radians
- All panel insert locations mapped (< 0.02 mm)
- Equipment thermo-elastic expansion
 - Tight tolerance hole and slotted hole specified
 - Controls direction of expansion
 - Limits uncertainty of unit location
 - Large unit expansion causes 10^{-12} m/s² change



Balancing the Gravity Field

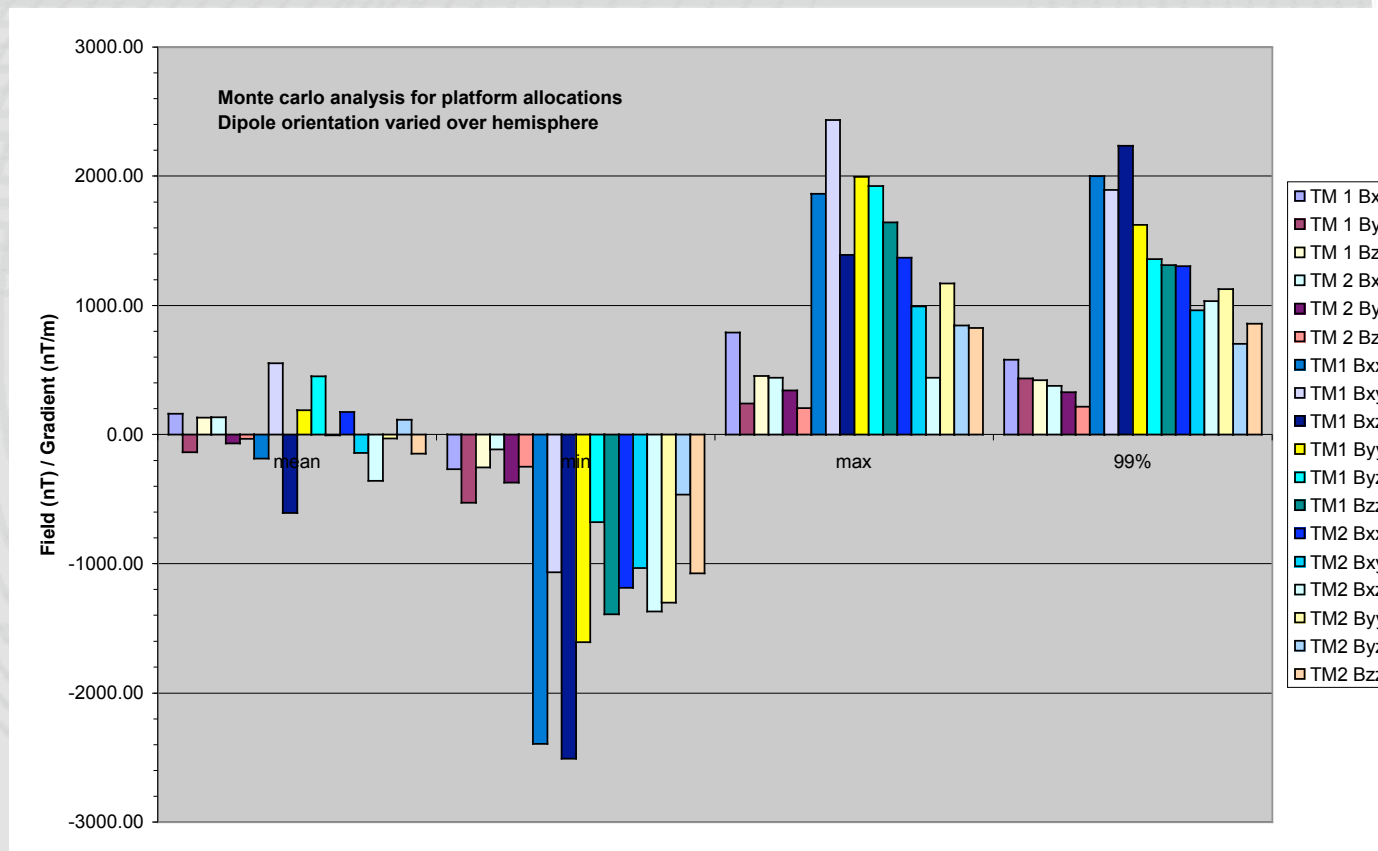
- Compensation mass minimised when close to TMs
 - Three levels of compensation masses
 - LTP Internal (mounting inside vacuum housing)
 - LTP External (mounted on vacuum housing)
 - Spacecraft Level (mounted on central cylinder)
- Spacecraft Level Compensation Masses
 - Series of fixed locations defined
 - Sets of different sized CMs available
 - Search algorithm finds sets of CMs to provide correction
 - Analysis shows that $\sim 1 \times 10^{-9} \text{ m/s}^2$ differential DC force correction can be achieved

Magnetic Field Disturbance Sources

- Budget allocation of $12 \times 10^{-15} \text{ m/s}^2/\sqrt{\text{Hz}}$
- Disturbances generated by field and field gradient due to S/C sources and interaction with interplanetary field
 - Interaction of field gradient fluctuations within the MBW with permanent and induced DC magnetisation
 - Interaction of fluctuating part of induced magnetisation within the MBW with DC field gradient
 - Mixing of high frequency magnetic field fluctuations above MBW, resulting in low frequency modulation
 - Fluctuating moment in TM due to interaction with interplanetary field, interacting with DC field gradient
- S/C Requirements: Field: 5000 nT; Gradient: 2830 nT/m

Equipment Level Magnetic Field Requirements

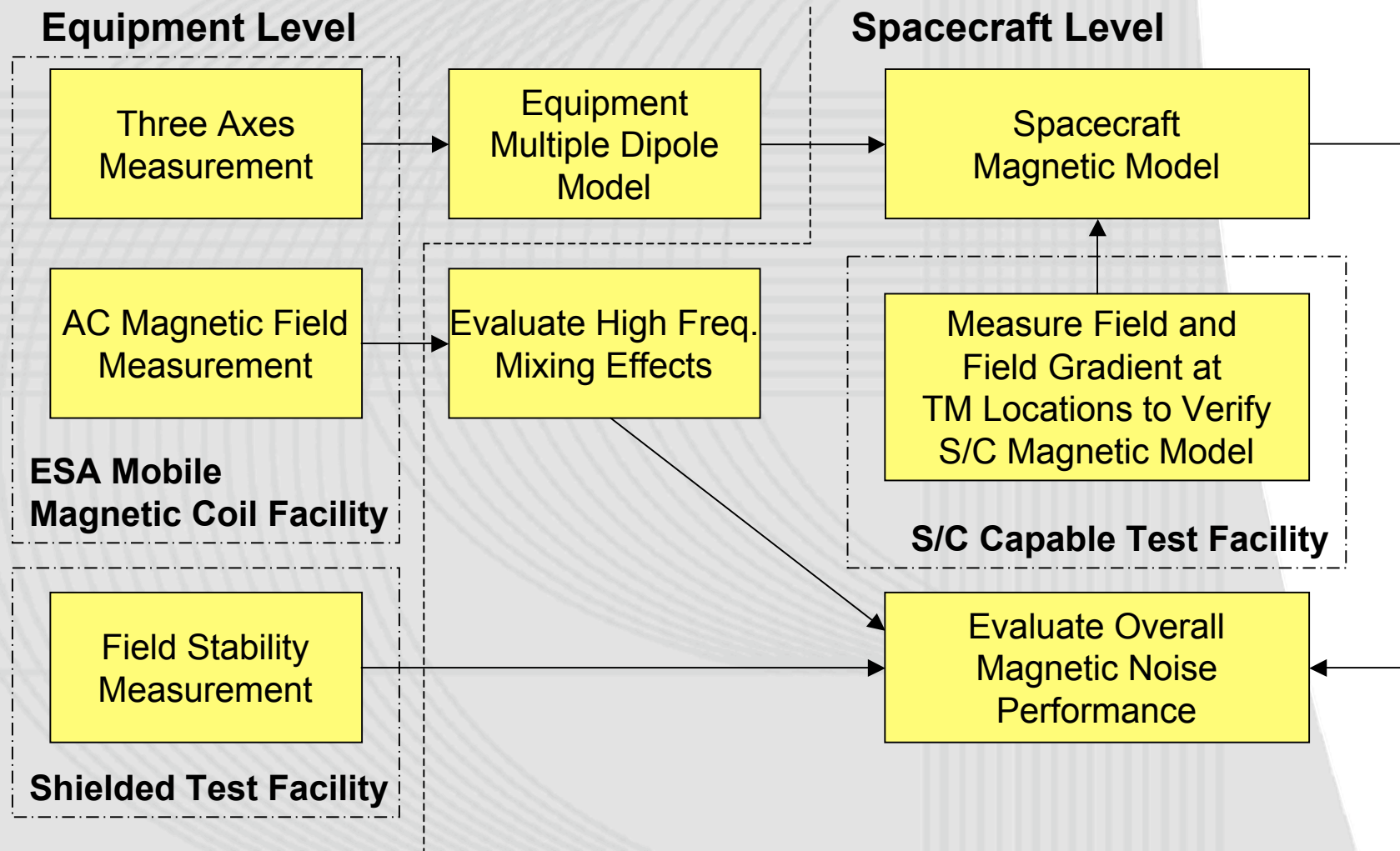
- Equipment level magnetic moment requirement set using historical data, complexity and proximity to TMs



Design Approach to Control Magnetic Disturbances

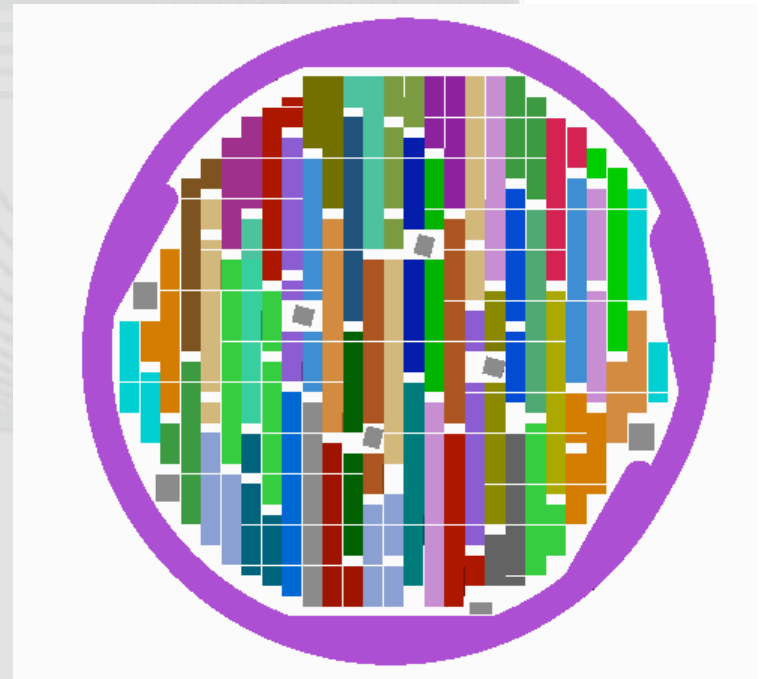
- Most effective method to control by design:
 - Avoid permanent magnets, assemblies that intentionally generate magnetic fields (relays, solenoids, etc.)
 - Appropriate selection of materials - no ferromagnetic parts
 - Minimise current levels as far as practical
 - Minimise loop area on circuit boards and harness by keeping return lines in close proximity to out-going lines
 - Avoid unintended current loops - single-point grounding, careful design of power distribution systems

Magnetic Testing



Solar Array Design

- Solar array is physically large and close to TMs
 - Not possible to use overall magnetic moment in model
 - Measurement of magnetic dipole not practical
 - Magnetic properties are entirely calculated
- Array design will be optimised to minimise magnetic field and field gradient

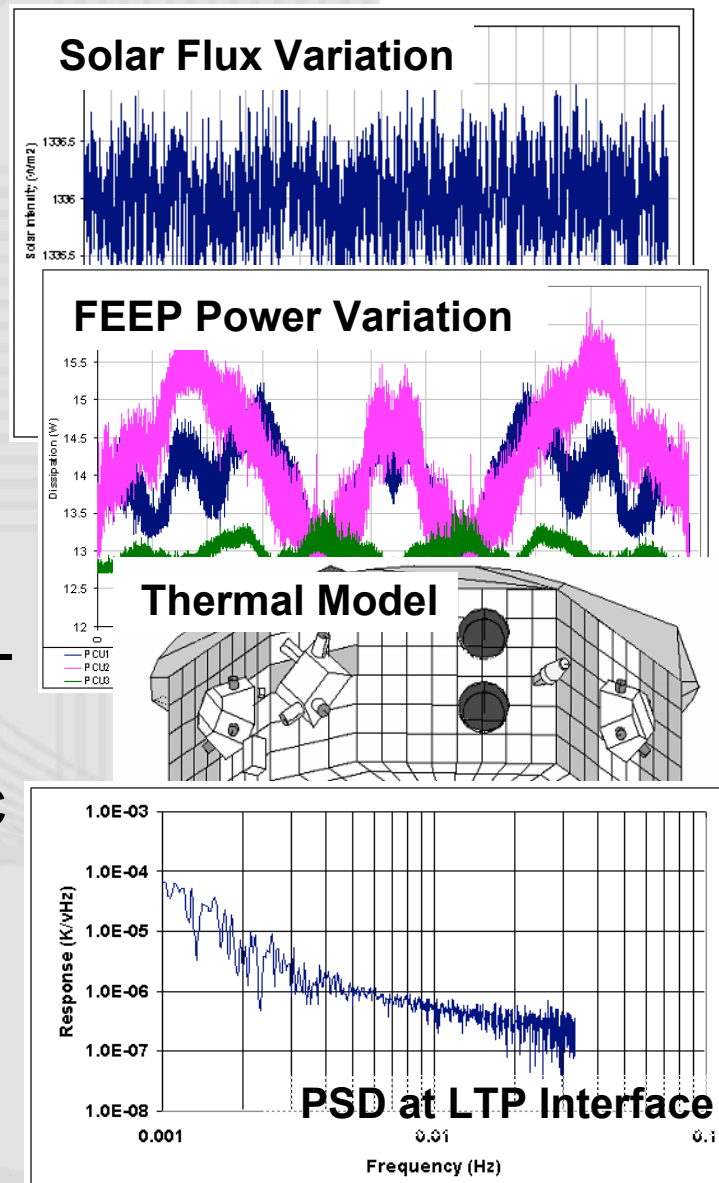


Thermal Effects

- Temperature fluctuations between S/C and LTP
 - Thermal distortion of housing and optical bench
 - Effects induced by thermal gradient across sensor housing
 - Temperature stability requirement 10^{-3} K/ $\sqrt{\text{Hz}}$
- Self-gravity noise cause by thermo-elastic effects
 - Rigid-body motion of the LTP due to thermo-elastic distortions at the S/C-LTP interface
 - Causes gravity field at TMs to vary generating an acceleration noise
 - Acceleration noise requirement – 2.12×10^{-15} m/s²/ $\sqrt{\text{Hz}}$
 - Translational distortion requirement – 10 nm/ $\sqrt{\text{Hz}}$

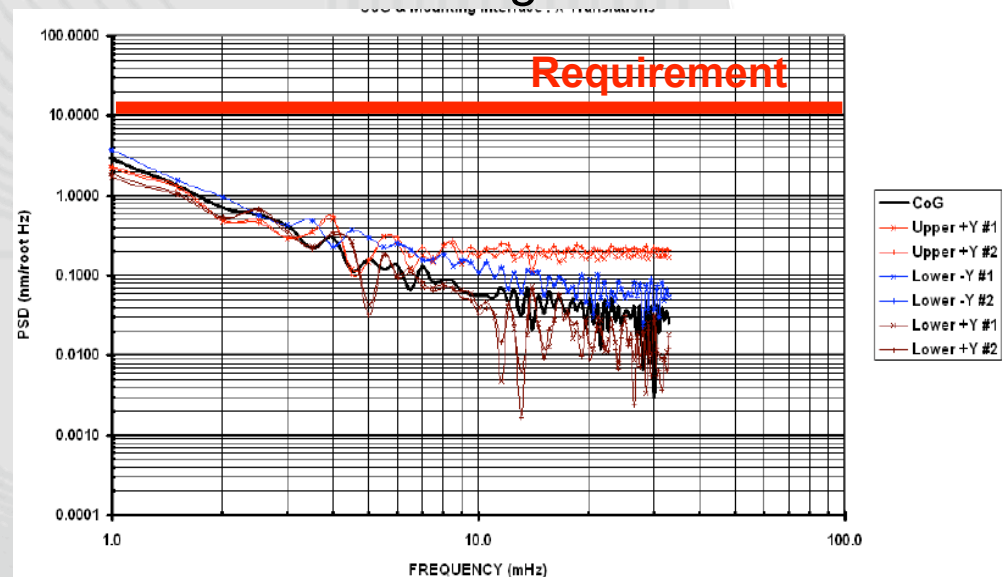
Thermal Stability

- Variation in solar flux generates noise
 - Heat fluctuations on array transmitted through structure to payload interface
 - Via DFACS which controls the attitude, causing power dissipation variations in micro-propulsion elements
- S/C thermal capacity acts as a low-pass filter
 - High frequency sources damped by S/C resistance to temperature change



Thermo-Elastic Distortion Analysis

- Input - Thermal stability analysis time histories
 - Temperature distribution mapped to FE mesh of SCM structure model
 - Thermal distortion analysis— generation of distortion time histories at LCA geometric centre and S/C LCA interface
 - PSD calculated by applying Fourier transforms to grid time histories
- A structure level thermal distortion test will be used to correlate the thermo-elastic model



Conclusions

- The impact of spacecraft level disturbances is controlled on LPF by a combination of:
 - Setting of appropriate requirements to limit or eliminate effects
 - Modelling of the disturbances
 - Testing to verify models, where feasible

Introduction to LISA Pathfinder (LPF)

- LPF a technology demonstration mission
 - LISA Test Package (LTP)
 - Drag Free Attitude Control System (DFACS)
 - Micro-Propulsion Technologies
- Launch to low Earth orbit in late-2009
- Transfer to L1 using chemical propulsion stage
- L1 provides a benign operating environment

